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Subject:

2016 First Quarter Operation Maintenance and Monitoring Report,
Operable Unit 2, Northrop Grumman Systems Corporation and Naval Weapons
Industrial Reserve Plant (NWIRP) Sites, Bethpage, New York.
(NYSDEC Site #s 1-30-003A and B)

Dear Henry and Steve:

On behalf of Northrop Grumman Systems Corporation (Northrop Grumman), Arcadis is providing the NYSDEC with the 2016 First Quarter Operation Maintenance and Monitoring Report (Report). This Report was prepared to document the operation, maintenance, and monitoring (OM&M) activities conducted for the on-site portion of the Operable Unit 2 (OU2) groundwater remedy and the results of ongoing volatile organic compound (VOC) and inorganic monitoring in groundwater to meet the remedial objectives set forth in the March 2001 OU2 Record of Decision (ROD).

Table 1 summarizes OU2 remedial system performance operational data and water balance. Tables 2 and 3 provide the analytical results for remedial system water samples for this period. Tables 3, 4 and 5 provide the analytical results and analysis for vapor samples collected from the system for this period. Figures 1 through 3 show the Well and Treatment System Site Locations, Treatment System Site Plan and the Treatment System Schematic, respectively.

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May 31, 2016

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NY001496.315I.GWMI4

Mr. Henry Wilkie Mr. Steven Scharf, P.E. May 31, 2016

Please contact us if you have any questions or comments.

Sincerely,

Arcadis of New York, Inc.

David E. Stern Senior Hydrogeologist

Carlo San Giovanni Project Manager

Carlo Son Grovann.

Copies:

Ed Hannon - Northrop Grumman Fred Weber - Northrop Grumman Walter Parish - NYSDEC Region 1 Steven Karpinski - New York State Department of Health Michael Alarcon - Nassau County Department of Health Joseph DeFranco - Nassau County Department of Health Lora Fly - NAVFAC Midlant Environmental David Brayack - TetraTech NUS, Inc. Roger Smith - Glenn Springs Holdings, Inc. Kevin Lumpe - Steel Equities Thomas Taccone - USEPA Robert Alvey - USEPA Carol Stein-USEPA

Matthew Russo - Town of Oyster Bay Stan Carey - Massapequa Water District Matthew Snyder - New York American Water Charles Prucha – South Farmingdale Water District John Reinhardt - Town of Hempstead Water District Michael Boufis - Bethpage Water District

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Table 1
Operational Summary for the On-Site Portion of the OU2 Groundwater Remedy, First Quarter 2016 (1)
Operable Unit 2, Northrop Grumman Systems Corporation,
Bethpage, New York



| | 6.6666 | e Rates (gott) | | nartery Flow Volumes N | | Characa y 790 co | | 70 to Massa Ro | HOVES INC. |
|---|--------------------------------------|------------------------------|-------------------|-----------------------------------|--------------|------------------|------------|----------------|-----------------------------|
| | Design | Average | Design | Assis | | 762 | 7.0 | Content | Constitution (Constitution) |
| Inition Croundvaler | | | | | | | | | |
| Well 1 ⁽¹¹⁾ | 800 | 853 | 104.8 | 105.1 | 100% | 792 | 840 | 738 | 41,596 |
| Well 3R ⁽¹¹⁾ | 700 | 971 | 91.7 | 119.7 | 131% | 529 | 580 | 568 | 87,383 |
| Well 17 ⁽¹²⁾ | 1,000 | 1,020 | 131.0 | 125.7 | 96% | 149 | 190 | 195 | 51,929 |
| Well 18 ^(12,13) | 600 | 700 | 78.6 | 87.1 | 111% | 51 | 72 | 51 | 5,948 |
| Well 19 ⁽¹²⁾ | 700 | 729 | 91.7 | 92.6 | 101% | 148 | 180 | 136 | 7,571 |
| Total (14) | 3,800 | 4,273 | 498 | 530 | 106% | | | 1,688 | 194,427 |
| | | | | | | | | | |
| | | | | | | | | | |
| Effluent Groundwater ⁶ | | | | | | | | | |
| Calpine | 100 - 400 | 122 | | 15.5 | | | | | |
| | 100 - 400 2 - 42 | 122 0 | | 15.5 0 | | | | | |
| Calpine | | | | | | | | | |
| Calpine OXY Biosparge ⁽¹⁰⁾ | 2 - 42 | 0 | | 0 | | | | | |
| Calpine OXY Biosparge ⁽¹⁰⁾ West Recharge Basins | 2 - 42 1,112 - 1,455 | 0 1,045 | | 0 136.9 | | | 2.1 | | |
| Calpine OXY Biosparge ⁽¹⁰⁾ West Recharge Basins South Recharge Basins | 2 - 42 1,112 - 1,455 2,231 | 0 1,045 2,883 | 292.4 | 0 136.9 377.8 | 129% | | 2.1 | | |
| Calpine OXY Biosparge (10) West Recharge Basins South Recharge Basins Total (14) Additional Flow to South Recharge Basins | 2 - 42 1,112 - 1,455 2,231 | 0 1,045 2,883 | 292.4 | 0 136.9 377.8 | 129% | | 2.1 | | |
| Calpine OXY Biosparge (10) West Recharge Basins South Recharge Basins Total (14) Auditional Flow to South Recharge Basins Storm Water Runoff Contributing to South Recharge | 2 - 42 1,112 - 1,455 2,231 | 0 1,045 2,883 | 292.4 | 0 136.9 377.8 | 129% | | 2.1 | | |
| Calpine OXY Biosparge (10) West Recharge Basins South Recharge Basins Total (14) Additional Flow to South Recharge Basins | 2 - 42 1,112 - 1,455 2,231 | 0 1,045 2,883 4,050 | 292.4 | 0 136.9 377.8 530 | 129% | | 2.1 1.6 | | |

| Treatment Efficiencies (*) | |
|----------------------------|--------|
| Tower 96 System: | 99.6% |
| Tower 102 System: | >99.9% |
| | |

Operational Summary for the On-Site Portion of the OU2 Groundwater Remedy, First Quarter 2016 (1)
Operable Unit 2, Northrop Grumman Systems Corporation,
Bethpage, New York



Notes and Abbreviations:

- (1) Quarterly reporting period: January 04, 2016 through April 04, 2016.
- "Design" flow rates were determined for the five remedial wells and for the South Recharge Basins based on computer modeling (ARCADIS G&M, Inc. 2003c, modified in April 2005). Flow rates for Calpine, OXY Biosparge and West Recharge Basins are typical flow rates and are provided for reader information. "Design" flow volumes represent the volume of water that should be pumped/discharged during the reporting period and is calculated by multiplying the design rate by the reporting period duration.
- "Average" flow rates for the remedial wells represent the average actual pumping rates when the pumps are operational and do not take into account the time that a well is not operational. During this quarterly reporting period, the remedial wells operated for the following percentage of the time: Well 1 (94%), Well 3R (94%), Well 17 (94%), Well 18 (95%), and Well 19 (97%). "Actual" volumes are determined via totalizing flow meters.
- "Average" flow rates for the system discharges represent the average flow rate during the entire reporting period and are determined by dividing the reporting period by the reporting period duration. The Calpine and South Recharge Basins flow volumes are determined via totalizing flow meters. The West Recharge Basin flow is calculated by subtracting the cumulative flow to the other discharges from the total influent flow. Actual flow to the recharge basins is greater, as shown, because storm water combines with the plant effluent prior to discharge to the recharge basins.
- (5) The TCE and TVOC concentrations for the remedial wells are from the quarterly sampling event performed during this reporting period on March 14, 2016 (Table 2).
- (6) The TVOC concentration for the two sets of recharge basins are their respective average monthly SPDES concentration for the current quarter.
- (7) TVOC mass removed for the reporting period is calculated by multiplying the TVOC concentration from the quarterly sampling event and the quantity of water pumped during the reporting period.
- (8) There are four discharges for the effluent groundwater: South Recharge Basins, West Recharge Basins, Calpine and OXY Biosparge system. Treated water is continuously discharged to the south and west recharge basins, and is available "on-demand" to both the Calpine Power Plant (Calpine) for use as make-up water, and the biosparge remediation system operated by Occidental Chemical (OXY Biosparge).
- 9) Treatment System Efficiencies are calculated by dividing the difference between the remedial well flow weighted influent and effluent TVOC concentrations by the remedial well flow weighted influent concentration.
- (10) Occidental Chemical reported that the OXY Biosparge system required no usage in the 1st Quarter of 2016.
- (11) Wells 1 and 3R were shut down on February 10, 2016 for replacement of the Occidental blower belt at Tower 96 and from March 3 through March 7, 2016 for replacement of the heat exchanger steam coil at Tower 96.
- (12) Wells 17, 18 and 19 shut down on February 7, 2016 and on March 6, 2016 due to power failures.
- (13) Well 18 was shut down on February 3, 2016 for modification of the Variable Frequency Drive.
- (14) Total pumpage/recharge rates are accurate to ±15% due to limitations in metering. Flow meter calibration was completed at all required locations except the Tower 102 Weir Overflow (South Recharge Basins), which is scheduled.
- (15) Storm Water Runoff Volume is calculated by multiplying the adjusted tributary area and NOAA precipitation data for the reporting periods. The adjusted tributary area is tributary area is tributary area at that is adjusted by the runoff coefficient to exclude the infiltration volume from the total rainfall volume. The tributary area, runoff coefficient, and adjusted tributary area are from Dvirka and Bartilucci Consulting Engineers' Storm Water Permit Evaluation Report (January, 28, 2010). The NOAA precipitation data are calculated as a sum of NOAA daily precipitation data for the reporting period. NOAA precipitation data are retrieved from Station GHCND:USW00054787 FARMINGDALE REPUBLIC AIRPORT, NY US.
- (16) Total Flow Volume to South Recharge Basins is estimated as a sum of flow volumes contributed from the Effluent Groundwater to South Recharge Basins and from Storm Water Runoff to South Recharge Basins.

| | not applicable | NOAA | National Oceanic and Atmospheric Administration |
|------|----------------------|-------|---|
| μg/L | micrograms per liter | SPDES | State Pollution Discharge Elimination System |
| gpm | gallons per minute | TCE | trichloroethene |
| lbs | pounds | TVOC | total volatile organic compounds |
| MG | million gallons | VOC | volatile organic compounds |

Table 2
Concentrations of Constituents in Remedial Wells and
Treatment System Effluents, First Quarter 2016, Operable Unit 2,
Northrop Grumman Systems Corporation,
Bethpage, New York



| | constant ID | WELL | WELLER | SEEFF CENT |
|--|---|-----------|-----------|-------------------|
| Constituents | Sample ID: | WELL 1 | WELL 3R | TOO ERFOLUENT (GW |
| units in ug/L) | Sample Date: | SIGNATURE | 371.02016 | 3114/2015 |
| | NYSDEC | | | |
| | SCGs | | | |
| Volatile Organic Compounds (VOCs) ^(1,2) | *************************************** | | | |
| I,1,1-Trichloroethane | 5 | 0.40 J | 0.80 J | < 1.0 |
| ,1,2,2-Tetrachloroethane | 5 | < 1.0 | < 1.0 | < 1.0 |
| ,1,2-Trichloroethane | 5 | < 1.0 | < 1.0 | < 1.0 |
| I,1-Dichloroethane | 5 | 0.82 J | 1.5 | < 1.0 |
| ,1-Dichloroethene | 5 | 2.4 | 4.0 | < 1.0 |
| ,2-Dichloroethane | 5 | < 1.0 | < 1.0 | < 1.0 |
| ,2-Dichloropropane | 5 | 4.2 | < 1.0 | < 1.0 |
| 2-Butanone (MEK) | 50 | < 10 | < 10 | < 10 |
| -Hexanone (MBK) | 50 | < 5.0 | < 5.0 | < 5.0 |
| -methyl-2-pentanone (MIK) | 50 | < 5.0 | < 5.0 | < 5.0 |
| Acetone | 50 | < 10 | < 10 | < 10 |
| Benzene | 1 | < 0.50 | < 0.50 | < 0.50 |
| Bromodichloromethane | 50 | < 1.0 | < 1.0 | < 1.0 |
| Bromoform | 50 | < 1.0 | < 1.0 | < 1.0 |
| Bromomethane | 5 | < 2.0 | < 2.0 | < 2.0 |
| Carbon Disulfide | 50 | < 2.0 | < 2.0 | < 2.0 |
| Carbon tetrachloride | 5 | < 1.0 | < 1.0 | < 1.0 |
| Chlorobenzene | 5 | < 1.0 | < 1.0 | < 1.0 |
| Chloroethane | 5 | < 1.0 | < 1.0 | < 1.0 |
| Chloroform | 7 | 0.24 J | < 1.0 | < 1.0 |
| Chloromethane | 5 | < 1.0 | < 1.0 | < 1.0 |
| is-1,2-dichloroethene | 5 | 4.9 | 5.6 | < 1.0 |
| is-1,3-dichloropropene | 5 | < 1.0 | < 1.0 | < 1.0 |
| Dibromochloromethane | 5 | < 1.0 | < 1.0 | < 1.0 |
| Ethylbenzene | 5 | < 1.0 | < 1.0 | < 1.0 |
| Methylene Chloride | 5 | < 2.0 | < 2.0 | < 2.0 |
| Styrene | 5 | < 1.0 | < 1.0 | < 1.0 |
| etrachloroethene | 5 | 30 | 31 | < 1.0 |
| oluene | 5 | < 1.0 | < 1.0 | < 1.0 |
| rans-1,2-dichloroethene | 5 | < 1.0 | < 1.0 | < 1.0 |
| rans-1,3-dichloropropene | 5 | < 1.0 | < 1.0 | < 1.0 |
| richloroethylene | 5 | 792 D | 529 D | 2.6 |
| richlorotrifluoroethane (Freon 113) | 5 | 3.3 J | 3.6 J | < 5.0 |
| /inyl Chloride | 2 | < 1.0 | 8.6 | < 1.0 |
| (ylene-o | 5 | < 1.0 | < 1.0 | < 1.0 |
| (ylenes - m,p | 5 | < 1.0 | < 1.0 | < 1.0 |
| Total VOCs ⁴¹ | ř | 840 | 580 | 2.6 |

Table 2
Concentrations of Constituents in Remedial Wells and
Treatment System Effluents, First Quarter 2016, Operable Unit 2,
Northrop Grumman Systems Corporation,
Bethpage, New York



| | Location ID | WELL IN | WELLT | 9450.00 | 102 EFF 1EA |
|--|-----------------------|-----------|----------|-----------|-------------|
| onstituente | Sample ID: | MELL | 99511.18 | WELL 19 | (200 |
| units in ligit.) | Sample Date: | 3/14/2016 | 3142016 | 3114/2016 | 0.000 |
| | NYSDEC | | | | |
| 4.2 | SCGs | | | | |
| Volatile Organic Compounds (VOCs) ^(1,2) | (µg/L) ⁽³⁾ | | | | |
| ,1,1-Trichloroethane | 5 | 0.45 J | 0.64 J | 0.40 J | < 1.0 |
| ,1,2,2-Tetrachloroethane | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| ,1,2-Trichloroethane | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| ,1-Dichloroethane | 5 | 1.0 | 1.3 | 0.77 J | < 1.0 |
| ,1-Dichloroethene | 5 | 2.1 | < 1.0 | 0.79 J | < 1.0 |
| ,2-Dichloroethane | 5 | < 1.0 | < 1.0 | 0.39 J | < 1.0 |
| ,2-Dichloropropane | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| -Butanone (MEK) | 50 | < 10 | < 10 | < 10 | < 10 |
| -Hexanone (MBK) | 50 | < 5.0 | < 5.0 | < 5.0 | < 5.0 |
| -methyl-2-pentanone (MIK) | 50 | < 5.0 | < 5.0 | < 5.0 | < 5.0 |
| cetone | 50 | < 10 | < 10 | < 10 | < 10 |
| Benzene | 1 | < 0.50 | < 0.50 | < 0.50 | < 0.50 |
| Bromodichloromethane | 50 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| Bromoform | 50 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| Bromomethane | 5 | < 2.0 | < 2.0 | < 2.0 | < 2.0 |
| Carbon Disulfide | 50 | < 2.0 | < 2.0 | < 2.0 | < 2.0 |
| Carbon tetrachloride | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| Chlorobenzene | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| Chloroethane | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| Chloroform | 7 | 0.38 J | 0.23 J | 0.45 J | < 1.0 |
| Chloromethane | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| is-1,2-dichloroethene | 5 | 3.5 | 2.2 | 18 | < 1.0 |
| is-1,3-dichloropropene | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| Dibromochloromethane | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| thylbenzene | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| Nethylene Chloride | 5 | < 2.0 | < 2.0 | < 2.0 | < 2.0 |
| Styrene | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| etrachloroethene | 5 | 29 | 14 | 7.3 | < 1.0 |
| oluene | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| rans-1,2-dichloroethene | 5 | < 1.0 | < 1.0 | 0.90 J | < 1.0 |
| rans-1,3-dichloropropene | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| richloroethylene | 5 | 149 | 51 | 148 | < 1.0 |
| richlorotrifluoroethane (Freon 113) | 5 | 5.0 | 1.8 J | 1.2 J | < 5.0 |
| /inyl Chloride | 2 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| (ylene-o | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| (ylenes - m,p | 5 | < 1.0 | < 1.0 | < 1.0 | < 1.0 |
| otal VOCs ^{al} | 3 | 190 | 72 | 180 | 0 |

Table 2

Concentrations of Constituents in Remedial Wells and Treatment System Effluents, First Quarter 2016, Operable Unit 2, Northrop Grumman Systems Corporation, Bethpage, New York



Notes and Abbreviations:

- (1) VOC samples analyzed using USEPA Method 8260C. 1,4-Dioxane samples analyzed using USEPA Method 8270 SIM.
- (2) Results for the program are validated at 20% frequency, per protocols specified in OU2 Groundwater Monitoring Plan (Arcadis 2014).
- (3) Standards, Criteria, and Guidance (SCG) values based on documents referenced in the Groundwater Feasibility Study Report (ARCADIS Geraghty & Miller, Inc. 2000) that are based on the NYSDEC TOGs (NYSDEC 1998); most stringent values are listed.
- (4) Total VOC results rounded to two significant figures.
- (5) A blind replicate sample was taken at Well 19 and analyzed for 1,4-Dioxane with a detection of 4.53 ug/L.

Compound detected in exceedance of NYSDEC SCG Criteria.

2.4 Bold value indicates a detection.

< 5.0 Compound is not detected above its laboratory quantification limit.

μg/L micrograms per liter

D Concentration is based on a diluted sample analysis.

J Constituent value is estimated.

NYSDEC New York State Department of Conservation

NS None Specified REP blind replicate sample

SCG standards, criteria and guidance value

SIM selective ion monitoring VOC volatile organic compounds

Table 3 Vapor Sample Analytical Results for Treatment Systems, First Quarter 2016, Northrop Grumman Systems Corporation, Operable Unit 2, Bethpage, New York



| ocation B | | | | | |
|--------------------|-----------|---|-------------|--|--|
| | | A CONTRACTOR | | | |
| Saltine | | | | | 2.4 |
| Date | 3/14/2016 | 314211 | 3/14/2016 | 3/14/2016 | 3/14/2016 |
| Cs) ⁽¹⁾ | | | | | |
| | 24 | 7.6 | < 0.55 | 18 | < 0.55 |
| | < 14 | < 3.2 | < 0.69 | < 2.7 | < 0.69 |
| | < 11 | < 2.6 | < 0.55 | < 2.2 | < 0.55 |
| | 53 | 37 | 4.5 | 54 | 6.1 |
| | 164 | 124 | 21 | 129 | 28 |
| | < 16 | < 3.8 | < 0.81 | 4.0 | < 0.81 |
| | 103 | 13 | < 0.92 | < 3.7 | < 0.92 |
| | < 13 | < 3.0 | < 0.64 | < 2.6 | < 0.64 |
| | < 13 | < 3.1 | < 0.67 | < 2.7 | < 0.67 |
| | < 8.3 | < 2.0 | < 0.41 | < 1.7 | < 0.41 |
| | < 16 | < 3.7 | < 0.78 | < 3.1 | < 0.78 |
| | < 12 | < 2.9 | < 0.62 | < 2.5 | 0.50 J |
| | < 5.0 | < 1.2 | < 0.25 | 4.8 | < 0.25 |
| | < 18 | < 4.3 | < 0.92 | < 3.7 | < 0.92 |
| | 9.2 J | 7.1 | 7.4 | < 2.1 | < 0.53 |
| | 11 J | 5.9 | < 0.98 | 17 | 1.0 |
| | < 8.3 | 1.3 J | 2.7 | 1.2 J | 1.3 |
| | < 18 | < 4.3 | < 0.91 | < 3.6 | < 0.91 |
| | < 18 | < 4.0 | < 0.85 | < 3.4 | < 0.85 |
| | < 17 | < 4.1 | < 0.87 | < 3.5 | < 0.87 |
| | < 14 | < 3.3 | 2.3 | < 2.8 | < 0.69 |
| | < 17 | < 4.0 | < 0.85 | < 3.4 | < 0.85 |
| | 1,580 | 50 | 1.2 | 674 | 1.8 |
| | < 15 | 6.0 | < 0.75 | 1.8 J | < 0.75 |
| | < 18 | < 4.3 | < 0.91 | < 3.6 | < 0.91 |
| | 22,500 D | 3,800 D | 9.1 | 5,700 D | 31 |
| | 183 | 91 | < 0.77 | 113 | 7.4 |
| | 197 | 168 | 1.4 | < 0.41 | 0.54 |
| | 28 | < 4.1 | < 0.87 | < 3.5 | < 0.87 |
| | 39 | < 4.1 | < 0.87 | < 3.5 | < 0.87 |
| | Sample ID | Sample D. INFLUENT (AA) (AA) | Sample B: | Sample ID: INFLUENT AAA SEFELUENT AAA SAMPLE AAA S | Ca Ca |



Notes and Abbreviations:

Operable Unit 2, Bethpage, New York

(1) Vapor samples collected by ARCADIS on the dates shown and submitted to a NYSDOH ELAP certified laboratory for VOC

analyses per Modified USEPA Method TO-15.

(2) "Total VOCs" represents the sum of individual concentrations of compounds detected rounded to the nearest whole number.

24 Bold data indicates that the analyte was detected at or above its reporting limit.

D Concentration is based on a diluted sample analysis.

ELAP Environmental Laboratory Approval Program

J Compound detected below its reporting limit; value is estimated.

NYSDOH New York State Department of Health

USEPA United States Environmental Protection Agency

VOC volatile organic compound µg/m³ micrograms per cubic meter

Table 4A
Summary of SCREEN3 Model Input and Outputs
Tower 96 Treatment System, Operable Unit 2,
Northrop Grumman Systems Corporation,
Bethpage, New York



| Parameters | Date Sampled: 5/11/2015 | 0,072615 | 2/15/2015 | \$144720 (6) |
|--|-------------------------|----------|-----------|--------------|
| SCREEN3 Model Input | | | | |
| Source Type | Point | Point | Point | Point |
| Emission Rate (g/s) | 1 | 1 | 1 | 1 |
| Stack Height (ft) | 55 | 55 | 55 | 55 |
| Stack Height (m) | 16.8 | 16.8 | 16.8 | 16.8 |
| Stack Inside Diameter (m) | 0.508 | 0.508 | 0.508 | 0.508 |
| Air Flow Rate (scfm@stack temp) ⁽¹⁾ | 4,688 | 4,581 | 4,610 | 4,631 |
| Air Flow Rate (acfm) ^{(2), (3)} | 4,936 | 4,840 | 4,810 | 4,800 |
| Stack Gas Exit Temperature (K) ⁽²⁾ | 310 | 311 | 307 | 305 |
| Ambient Air Temperature (K) ⁽⁴⁾ | 287 | 293 | 275 | 277 |
| Receptor Height (m) ⁽⁵⁾ | 1.5 | 1.5 | 1.5 | 1.5 |
| Urban/Rural | Urban | Urban | Urban | Urban |
| Building Height (m) | 6.7 | 6.7 | 6.7 | 6.7 |
| Min Horizontal Bldg Dim (m) | 9.8 | 9.8 | 9.8 | 9.8 |
| Max Horizontal Bldg Dim (m) | 12.8 | 12.8 | 12.8 | 12.8 |
| Consider Bldg Downwash? | Yes | Yes | Yes | Yes |
| Simple/Complex Terrain Above Stack | Simple | Simple | Simple | Simple |
| Simple/Complex Terrain Above Stack Base | Simple | Simple | Simple | Simple |
| Meteorology | Full | Full | Full | Full |
| Automated Distances Array | Yes | Yes | Yes | Yes |
| Terrain Height Above Stack Base | 0 | 0 | 0 | 0 |
| SCREEN3 Model Output | | | | |
| 1-HR Max Concentration at Receptor Height (μg/m³) ⁽⁶⁾ | 195 | 199 | 196 | 198 |
| Annualization Factor ^(/) | 0.08 | 0.08 | 0.08 | 0.08 |
| Average Annual Concentration at Receptor Height (µg/m³) ⁽⁸⁾ | 15.6 | 15.9 | 15.7 | 15.8 |
| Distance To Max Concentration (m) ⁽⁹⁾ | 110 | 109 | 110 | 110 |
| | | | | |

Table 4A Summary of SCREEN3 Model Input and Outputs Tower 96 Treatment System, Operable Unit 2, Northrop Grumman Systems Corporation, Bethpage, New York



Notes and Abbreviations:

- (1) The stack air flow rate at the stack temperature (in scfm) was calculated by multiplying the stack air flow rate in acfm by the ratio of the standard temperature to the actual stack gas exit temperature in degrees Kelvin.
- (2) The stack air flow rate (in acfm) and temperature were measured using inline instrumentation. Values were measured at the blower effluent location.
- (3) The stack air flow rate is taken from the actual stack air flow rate on the day of sampling.
- (4) The ambient temperature was recorded from weather.newsday.com website for Islip, New York. The mean average temperature from the website was used in the model calculation.
- (5) The receptor height corresponds to the average inhalation level.
- (6) SCREEN3 calculated constituent concentration at listed conditions at the specified inhalation level.
- (7) A USEPA time averaging conversion factor of 1/0.08 was used to convert the 1-hour maximum concentration output to an annual average.
- (8) Average annual constituent concentration at the receptor height was calculated by multiplying the one hour maximum concentration by the annualization factor.
- (9) SCREEN3 calculated distance to the 1-hour maximum concentration.

μg/m³ micrograms per cubic meter acfm actual cubic feet per minute

ft feet

g/s grams per second

K Kelvin meters

scfm standard cubic feet per minute

USEPA United States Environmental Protection Agency

Table 4B
Summary of Air Emissions Model Output
Tower 96 Treatment System, Operable Unit 2,
Northrop Grumman Systems Corporation,
Bethpage, New York



| | | | Actual Efficient Con | central ones in the | |
|--------------------------------------|------------------------|---------|----------------------|---------------------|-----|
| Compound | | 5 1 2 2 | 8/8/2015 | 2.15.2016 | 4.2 |
| 1,1-Dichloroethane | 95,000 ⁽³⁾ | 0.57 | 34 | 5.3 | 4.5 |
| 1,1-Dichloroethene | 188,000 ⁽³⁾ | 2.3 | 60.7 | 56.7 | 21 |
| Chloroethane | 619,000 ⁽³⁾ | 12 | 13 | 8.2 | 7.4 |
| Chloroform | 150 | 0 | 2.5 | 0 | 0 |
| Chloromethane | 22,000 | 3.5 | 1.6 | 2.7 | 2.7 |
| Methylene Chloride | 14,000 | 1.7 | 1.7 | 0.87 | 2.3 |
| Tetrachloroethene | 300 | 2.7 | 0.37 | 0.61 | 1.2 |
| Trichloroethene | 14,000 | 32 | 3.8 | 9.7 | 9.1 |
| Trichlorotrifluoroethane (Freon 113) | 960,000 | 0 | 2.6 | 0 | 0 |
| Vinyl chloride | 180,000 | 1.0 | 28.4 | 44.5 | 1.4 |

Table 4B
Summary of Air Emissions Model Output
Tower 96 Treatment System, Operable Unit 2,
Northrop Grumman Systems Corporation,
Bethpage, New York



| | | | A III C | | |
|--------------------------------------|---------|----------|----------|------------|----------|
| Competed | | 0.00 | 10.00 | 0.01572015 | 44211 |
| 1,1-Dichloroethane | 0.63 | 1.73E+04 | 1.73E+04 | 1.77E+04 | 1.76E+04 |
| 1,1-Dichloroethene | 200 | 5.50E+06 | 5.51E+06 | 5.61E+06 | 5.59E+06 |
| Chloroethane | 10,000 | 2.75E+08 | 2.75E+08 | 2.81E+08 | 2.79E+08 |
| Chloroform | 14.7 | 4.05E+05 | 4.05E+05 | 4.12E+05 | 4.11E+05 |
| Chloromethane | 90 | 2.48E+06 | 2.48E+06 | 2.53E+06 | 2.51E+06 |
| Methylene Chloride | 60 | 1.65E+06 | 1.65E+06 | 1.68E+06 | 1.68E+06 |
| Tetrachloroethene | 4 | 1.10E+05 | 1.10E+05 | 1.12E+05 | 1.12E+05 |
| Trichloroethene | 0.2 | 5.50E+03 | 5.51E+03 | 5.61E+03 | 5.59E+03 |
| Trichlorotrifluoroethane (Freon 113) | 180,000 | 4.95E+09 | 4.96E+09 | 5.05E+09 | 5.03E+09 |
| Vinyl chloride | 0.068 | 1.87E+03 | 1.87E+03 | 1.91E+03 | 1.90E+03 |
| | | | | | |

Table 4B
Summary of Air Emissions Model Output
Tower 96 Treatment System, Operable Unit 2,
Northrop Grumman Systems Corporation,
Bethpage, New York



| Compound | | 514.174.15 | 919721015 | 57.57.115 | 3.6 4.2 6.5 | |
|--------------------------------------|---------|------------|-----------|-----------|-------------|-------|
| 1,1-Dichloroethane | 0.63 | 0.0% | 0.20% | 0.03% | 0.03% | 0.08% |
| 1,1-Dichloroethene | 200 | 0.0% | 0.0% | 0.0% | 0.0% | 0.00% |
| Chloroethane | 10,000 | 0.0% | 0.0% | 0.0% | 0.0% | 0.00% |
| Chloroform | 14.7 | 0.0% | 0.0% | 0.0% | 0.0% | 0.00% |
| Chloromethane | 90 | 0.0% | 0.0% | 0.0% | 0.0% | 0.00% |
| Methylene Chloride | 60 | 0.0% | 0.0% | 0.0% | 0.0% | 0.00% |
| Tetrachloroethene | 4 | 0.0% | 0.0% | 0.0% | 0.0% | 0.00% |
| Trichloroethene | 0.2 | 0.58% | 0.07% | 0.17% | 0.16% | 0.20% |
| Trichlorotrifluoroethane (Freon 113) | 180,000 | 0.0% | 0.0% | 0.0% | 0.0% | 0.00% |
| Vinyl chloride | 0.068 | 0.05% | 1.52% | 2.33% | 0.07% | 6.45% |
| | | | | | | |



Notes and Abbreviations:

- (1) Refers to the compound-specific SGC per the NYSDEC DAR-1 AGC/SGC tables revised February 28, 2014.
- (2) Only VOCs that were detected in the effluent vapor sample (T96 EFF) over the past year of system operation are included in this table.
- (3) An SGC was not provided in the DAR-1 AGC/SGC Tables, dated February 28, 2014. An interim SGC was developed based on guidelines provided in Section IV.A.2.b.1 of the NYSDEC DAR-1 Guidelines for the Control of Toxic Ambient Air Contaminants, 1991 edition.
- (4) AGC refers to the compound-specific annual guideline concentration per the NYSDEC DAR-1 AGC/SGC tables, revised February 28, 2014. NYSDEC DAR-1 AGCs were scaled using the results of a site-specific annual USEPA SCREEN 3 model to calculate the annual MASC per monitoring event.
- (5) Annual MASC was calculated by dividing the product of the AGC of a compound and the ratio of the SCREEN3 gas emission rate and the SCREEN 3 average annual concentration at receptor height by the air flow rate at the stack temperature and multiplying by the appropriate conversion factors.
- (6) Percent of MASC was calculated by dividing the actual effluent concentration by the MASC for the past four quarters of operation. Percentages have been rounded to two digits.
- (7) Cumulative percent of the MASC was calculated using a time-weighted average of the percent MASC per event. Percentages have been rounded to two digits.

μg/m³ micrograms per cubic meter
 0.57 bold value indicates a detection
 AGC annual guideline concentration
 DAR-1 Division of Air Resources-1

MASC maximum allowable stack concentration

NYSDEC New York State Department of Environmental Conservation

SGC short-term guideline concentration

Table 5A
Summary of SCREEN3 Model Input and Outputs
Tower 102 Treatment System, Operable Unit 2,
Northrop Grumman Systems Corporation,
Bethpage, New York



| Parameters | Pote Complete 67 (720)6 | | | 3 (1.77) |
|--|-------------------------|--------|--------|----------|
| SCREEN3 Model Input | | | | |
| Source Type | Point | Point | Point | Point |
| Emission Rate (g/s) | 1 | 1 | 1 | 1 |
| Stack Height (ft) | 69.52 | 69.52 | 69.52 | 69.52 |
| Stack Height (m) | 21.19 | 21.19 | 21.19 | 21.19 |
| Stack Inside Diameter (m) | 0.61 | 0.61 | 0.61 | 0.61 |
| Air Flow Rate (scfm@stack temp) ⁽¹⁾ | 8,068 | 7,930 | 7,655 | 7,873 |
| Air Flow Rate (acfm) ^{(2), (3)} | 8,220 | 8,080 | 7,800 | 8,000 |
| Stack Gas Exit Temperature (K) ⁽²⁾ | 300 | 300 | 300 | 299 |
| Ambient Air Temperature (K) ⁽⁴⁾ | 287 | 293 | 275 | 277 |
| Receptor Height (m) ⁽⁵⁾ | 1.5 | 1.5 | 1.5 | 1.5 |
| Jrban/Rural | Urban | Urban | Urban | Urban |
| Building Height (m) | 7.62 | 7.62 | 7.62 | 7.62 |
| Min Horizontal Bldg Dim (m) | 12.5 | 12.5 | 12.5 | 12.5 |
| Max Horizontal Bldg Dim (m) | 15.54 | 15.54 | 15.54 | 15.54 |
| Consider Bldg Downwash? | Yes | Yes | Yes | Yes |
| Simple/Complex Terrain Above Stack | Simple | Simple | Simple | Simple |
| Simple/Complex Terrain Above Stack Base | Simple | Simple | Simple | Simple |
| Meteorology | Full | Full | Full | Full |
| Automated Distances Array | Yes | Yes | Yes | Yes |
| Terrain Height Above Stack Base | 0 | 0 | 0 | 0 |
| SCREEN3 Model Output | | | | |
| 1-HR Max Concentration at Receptor Height (µg/m³) ⁽⁶⁾ | 108.7 | 110.6 | 114.3 | 111.3 |
| Annualization Factor ⁽⁷⁾ | 0.08 | 0.08 | 0.08 | 0.08 |
| Average Annual Concentration at Receptor Height (µg/m³ |) ⁽⁸⁾ 8.7 | 8.8 | 9.1 | 8.9 |
| Distance To Max Concentration (m) ⁽⁹⁾ | , 145 | 144 | 142 | 143 |



Notes and Abbreviations:

- (1) The stack air flow rate at the stack temperature (in scfm) was calculated by multiplying the stack air flow rate in acfm by the ratio of the standard temperature to the actual stack gas exit temperature in degrees Kelvin.
- (2) The stack air flow rate (in acfm) and temperature were measured using inline instrumentation. Values were measured at the blower effluent location.
- (3) The stack air flow rate is taken from the actual stack air flow rate on the day of sampling.
- (4) The ambient temperature was recorded from weather.newsday.com website for Islip, New York. The mean actual temperature from the website was used in the model calculation.
- (5) The receptor height corresponds to the average inhalation level.
- (6) SCREEN3 calculated constituent concentration at listed conditions at the specified inhalation level.
- (7) A USEPA time averaging conversion factor of 1/0.08 was used to convert the 1-hour maximum concentration output to an annual average.
- (8) Average annual constituent concentration at the receptor height was calculated by multiplying the one hour maximum concentration by the annualization factor.
- (9) SCREEN3 calculated distance to the 1-hour maximum concentration.

μg/m³ micrograms per cubic meter acfm actual cubic feet per minute

ft feet

g/s grams per second

K Kelvin meters

scfm standard cubic feet per minute

USEPA United States Environmental Protection Agency

Table 5B Summary of Air Emissions Model Output, Tower 102 Treatment System, Opearable Unit 2 Northrop Grumman Systems Corporation, Bethpage, New York



| | 30.0 | | and the second second | edition of the second | |
|-------------------------------------|------------------------|-------|-----------------------|-----------------------|------|
| Compound | | 5 (1) | 0/01/2015 | | |
| 1,1,1-Trichloroethane | 9,000 | 0.55 | 0 | 0 | 0 |
| 1,1-Dichloroethane | 95,000 ⁽³⁾ | 5.7 | 8.1 | 1.1 | 6.1 |
| 1,1-Dichloroethene | 188,000 ⁽³⁾ | 21 | 35 | 4.4 | 28 |
| Benzene | 1,300 | 0 | 0.51 | 0 | 0 |
| Carbon Disulfide | 6,200 | 0 | 0 | 0 | 0.5 |
| Chloroform | 150 | 1.6 | 1.6 | 0 | 1 |
| Chloromethane | 22,000 | 0.99 | 1.3 | 0.74 | 1.3 |
| Ethylbenzene | 20,700 ⁽³⁾ | 0 | 0.69 | 0 | 0 |
| Methylene Chloride | 14,000 | 1.3 | 1.5 | 3.1 | 0 |
| 「etrachloroethene | 300 | 1.6 | 3.7 | 0 | 1.8 |
| oluene | 37,000 | 0 | 21 | 0 | 0 |
| [richloroethene | 14,000 | 34 | 12 | 4.9 | 31 |
| richlorotrifluoroethane (Freon 113) | 960,000 | 7.1 | 7.7 | 0 | 7.4 |
| /inyl Chloride | 180,000 | 0 | 0 | 0 | 0.54 |
| Kylene-m,p | 22,000 | 0 | 1.9 | 0 | 0 |
| Xylene-o | 22,000 | 0 | 0.56 | 0 | 0 |

Table 5B Summary of Air Emissions Model Output, Tower 102 Treatment System, Opearable Unit 2 Northrop Grumman Systems Corporation, Bethpage, New York



| Compound | AGC ⁽⁴⁾ Annual MASC ⁽⁵⁾ (µg/m3) | | | | | | |
|--------------------------------------|---|----------|----------|----------|----------|--|--|
| | | 5.00 | 31323 | | | | |
| 1,1,1-Trichloroethane | 5,000 | 1.48E+08 | 1.49E+08 | 1.49E+08 | 1.49E+08 | | |
| 1,1-Dichloroethane | 0.63 | 1.87E+04 | 1.88E+04 | 1.88E+04 | 1.87E+04 | | |
| 1,1-Dichloroethene | 200 | 5.93E+06 | 5.96E+06 | 5.97E+06 | 5.95E+06 | | |
| 3enzene | 0.13 | 3.85E+03 | 3.87E+03 | 3.88E+03 | 3.87E+03 | | |
| Carbon Disulfide | 700 | 2.07E+07 | 2.09E+07 | 2.09E+07 | 2.08E+07 | | |
| Chloroform | 14.7 | 4.36E+05 | 4.38E+05 | 4.39E+05 | 4.37E+05 | | |
| Chloromethane | 90 | 2.67E+06 | 2.68E+06 | 2.69E+06 | 2.68E+06 | | |
| Ethylbenzene | 1,000 | 2.96E+07 | 2.98E+07 | 2.99E+07 | 2.98E+07 | | |
| Methylene Chloride | 60 | 1.78E+06 | 1.79E+06 | 1.79E+06 | 1.79E+06 | | |
| Tetrachloroethene | 4 | 1.19E+05 | 1.19E+05 | 1.19E+05 | 1.19E+05 | | |
| Toluene | 5,000 | 1.48E+08 | 1.49E+08 | 1.49E+08 | 1.49E+08 | | |
| Trichloroethene | 0.2 | 5.93E+03 | 5.96E+03 | 5.97E+03 | 5.95E+03 | | |
| Trichlorotrifluoroethane (Freon 113) | 180,000 | 5.33E+09 | 5.36E+09 | 5.37E+09 | 5.36E+09 | | |
| √inyl Chloride | 0.068 | 2.01E+03 | 2.03E+03 | 2.03E+03 | 2.02E+03 | | |
| Xylene-m,p | 100 | 2.96E+06 | 2.98E+06 | 2.99E+06 | 2.98E+06 | | |
| Xylene-o | 100 | 2.96E+06 | 2.98E+06 | 2.99E+06 | 2.98E+06 | | |

Table 5B
Summary of Air Emissions Model Output,
Tower 102 Treatment System, Opearable Unit 2
Northrop Grumman Systems Corporation,
Bethpage, New York



| | | | Recent of America States | | | Cumulative 25 MASC ²⁷ |
|--------------------------------------|---------|-------|--------------------------|-------|-------|-------------------------------------|
| Compound | | | | | | |
| 1,1,1-Trichloroethane | 5,000 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| 1,1-Dichloroethane | 0.63 | 0.03% | 0.04% | 0.01% | 0.03% | 0.03% |
| 1,1-Dichloroethene | 200 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Benzene | 0.13 | 0.0% | 0.01% | 0.0% | 0.0% | 0.003% |
| Carbon Disulfide | 700 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Chloroform | 14.7 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Chloromethane | 90 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Ethylbenzene | 1,000 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Methylene Chloride | 60 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Tetrachloroethene | 4 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Toluene | 5,000 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Trichloroethene | 0.2 | 0.57% | 0.20% | 0.1% | 0.52% | 0.31% |
| Trichlorotrifluoroethane (Freon 113) | 180,000 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Vinyl Chloride | 0.068 | 0.0% | 0.0% | 0.0% | 0.03% | 0.008% |
| Xylene-m,p | 100 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| Xylene-o | 100 | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |



Notes and Abbreviations:

- (1) Refers to the compound-specific SGC per the NYSDEC DAR-1 AGC/SGC tables revised February 28, 2014.
- (2) Only VOCs that were detected in the effluent vapor sample (T102 EFF) over the past year of system operation are included in this table.
- An SGC was not provided in the DAR-1 AGC/SGC Tables, dated February 28, 2014. An interim SGC was developed based on guidelines provided in Section IV.A.2.b.1 of the NYSDEC DAR-1 Guidelines for the Control of Toxic Ambient Air Contaminants, 1991 edition.
- (4) AGC refers to the compound-specific annual guideline concentration per the NYSDEC DAR-1 AGC/SGC tables, revised February 28, 2014. NYSDEC DAR-1 AGCs were scaled using the results of a site-specific annual USEPA SCREEN 3 model to calculate the annual MASC per monitoring event.
- (5) Annual MASC was calculated by dividing the product of the AGC of a compound and the ratio of the SCREEN3 gas emission rate and the SCREEN 3 average annual concentration at receptor height by the air flow rate at the stack temperature and multiplying by the appropriate conversion factors.
- (6) Percent of MASC was calculated by dividing the actual effluent concentration by the MASC for the past four quarters of operation. Percentages have been rounded to two digits.
- (7) Cumulative percent of the MASC was calculated using a time-weighted average of the percent MASC per event. Percentages have been rounded to two digits.

µg/m³ micrograms per cubic meter0.55 Bold value indicates a detection

-- Compound not reported, unable to compute MASC

AGC annual guideline concentration
DAR-1 Division of Air Resources-1

MASC maximum allowable stack concentration

NYSDEC New York State Department of Environmental Conservation

SCG short-term guideline concentration



